

# Mitigation of Induced Seismicity that is Triggered by Hydraulic Fracturing

Hamzeh Alimohammadi<sup>a</sup>, Mitchell Boyne<sup>a</sup>, David Eaton<sup>a</sup>, Zahra Esmaeilzadeh<sup>a</sup>, Edouard Kravchinsky<sup>b</sup>  
 University of Calgary<sup>a</sup>, University of Toronto<sup>b</sup>

## Introduction

We examine the current state of knowledge in evaluating hazards associated with hydraulic-fracturing induced seismicity; a particular focus is given to the Duvernay unconventional resource play in Alberta, Canada. The results of this study could be generalized for comparable unconventional resources in WCSB.

We aim to answer the following questions:

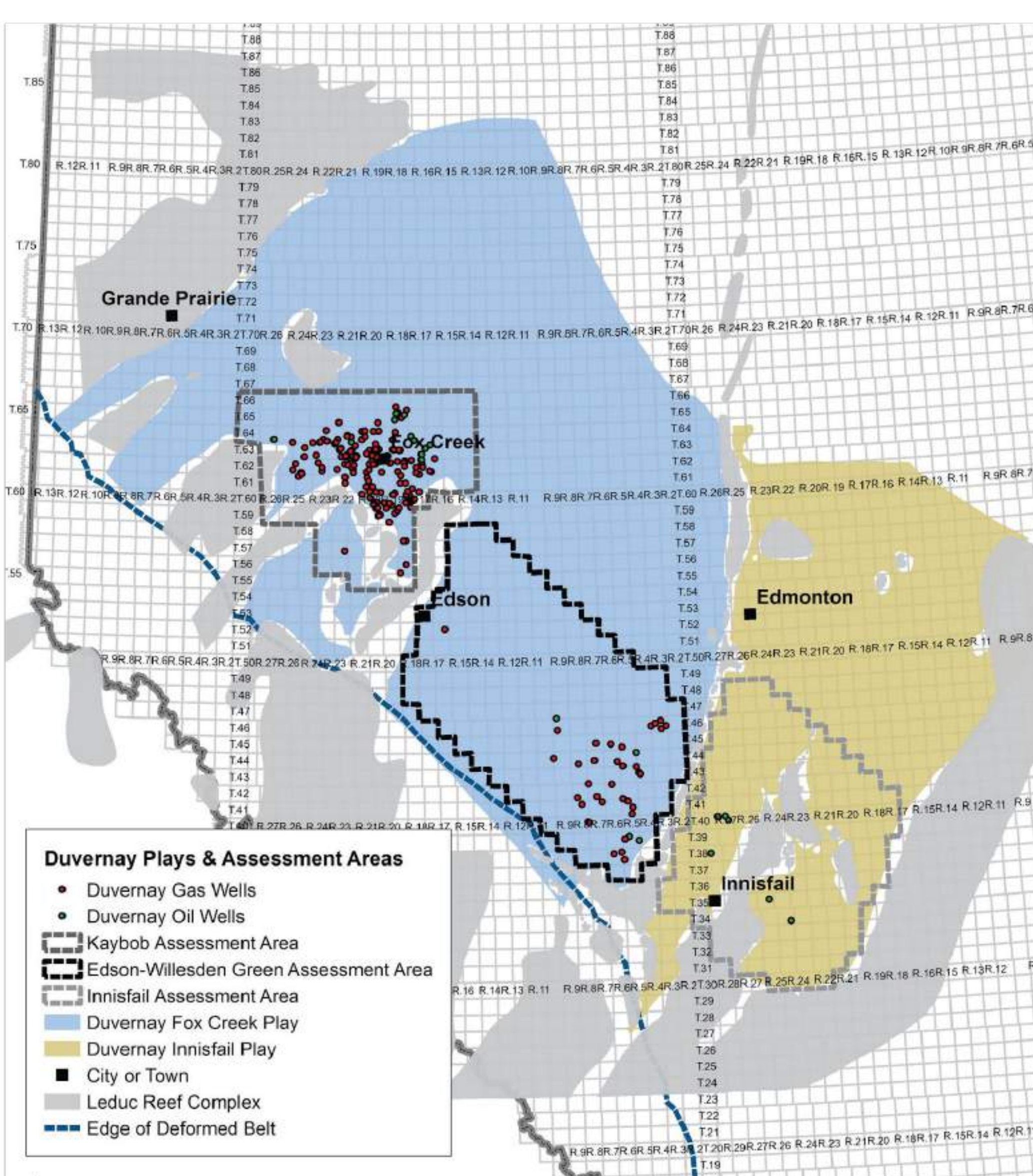
(1) What is the feasibility of quantifying geological susceptibility?

(2) With geomechanical modeling focus on:

- Critical orientation of faults in respect to the minimum and maximum stresses.
- Reactivation of fault due to stress / fluid pressure changes through hydraulic connectivity.
- Effectiveness of suggested mitigation methods.

This study offers insight into practices to minimize the risk of future induced seismicity.

## Geological Factors



The Duvernay unconventional resource play is geographically divided into the West Shale Basin or Fox Creek play (shown in blue) and the East Shale Basin, or Innisfail play (shown in yellow). Figure from Preston et al. (2016).

It is possible to minimize the risk of induced seismicity by considering/quantifying geological and hydrogeological parameters:

- Pre-existing faults
- In-situ stress conditions
- Pathways for pressure diffusion and/or stress transfer
- Rock geomechanical parameters
- Proximity to crystalline basement
- Formation overpressure
- Proximity to reef margins
- Lithium concentration
- Rates of natural seismicity
- Fluid injection volume

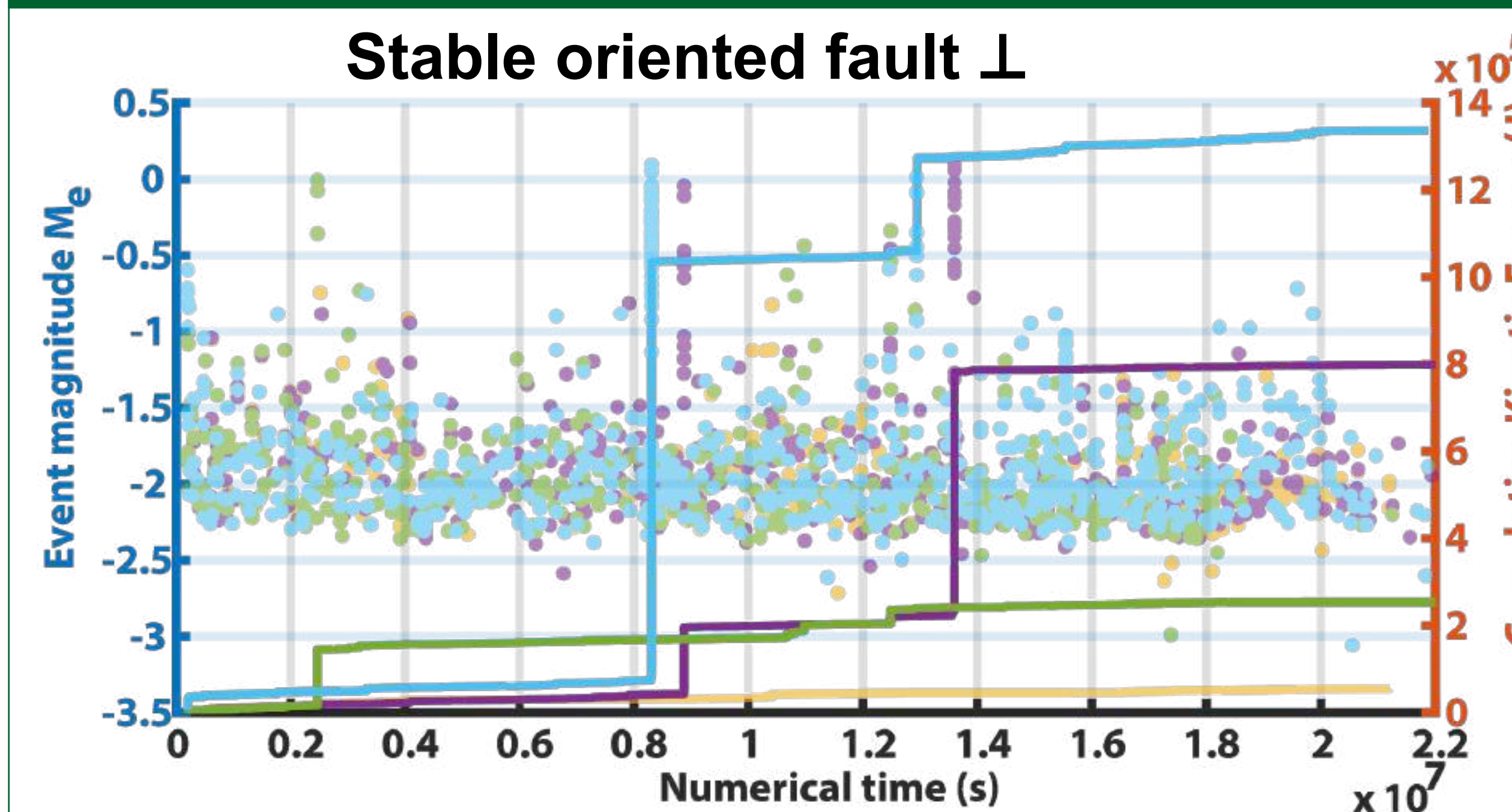
## Geomechanical Models

- Model using 2D finite-discrete element method (FDEM) Irazu software
- Fault is broken (no cohesion), dry (no fluids), assume strike-slip fault (vertical), coefficient of friction  $\mu=0.6$
- Rock mass (shale) is fraturable, homogeneous and isotropic
- Baseline model with 5 injection points away from fault
- $\sigma_{min} = 58 \text{ MPa}$ ,  $\sigma_{max} = 70 \text{ MPa}$  at  $\sim 3 \text{ km}$  (Lavoie et al., 2018)
- Fault orientation near critical  $\theta = \angle$  ( $30^\circ$  worst case) and stable  $\theta = \perp$  ( $90^\circ$  best case) from  $\sigma_{max}$

### Mitigation strategy

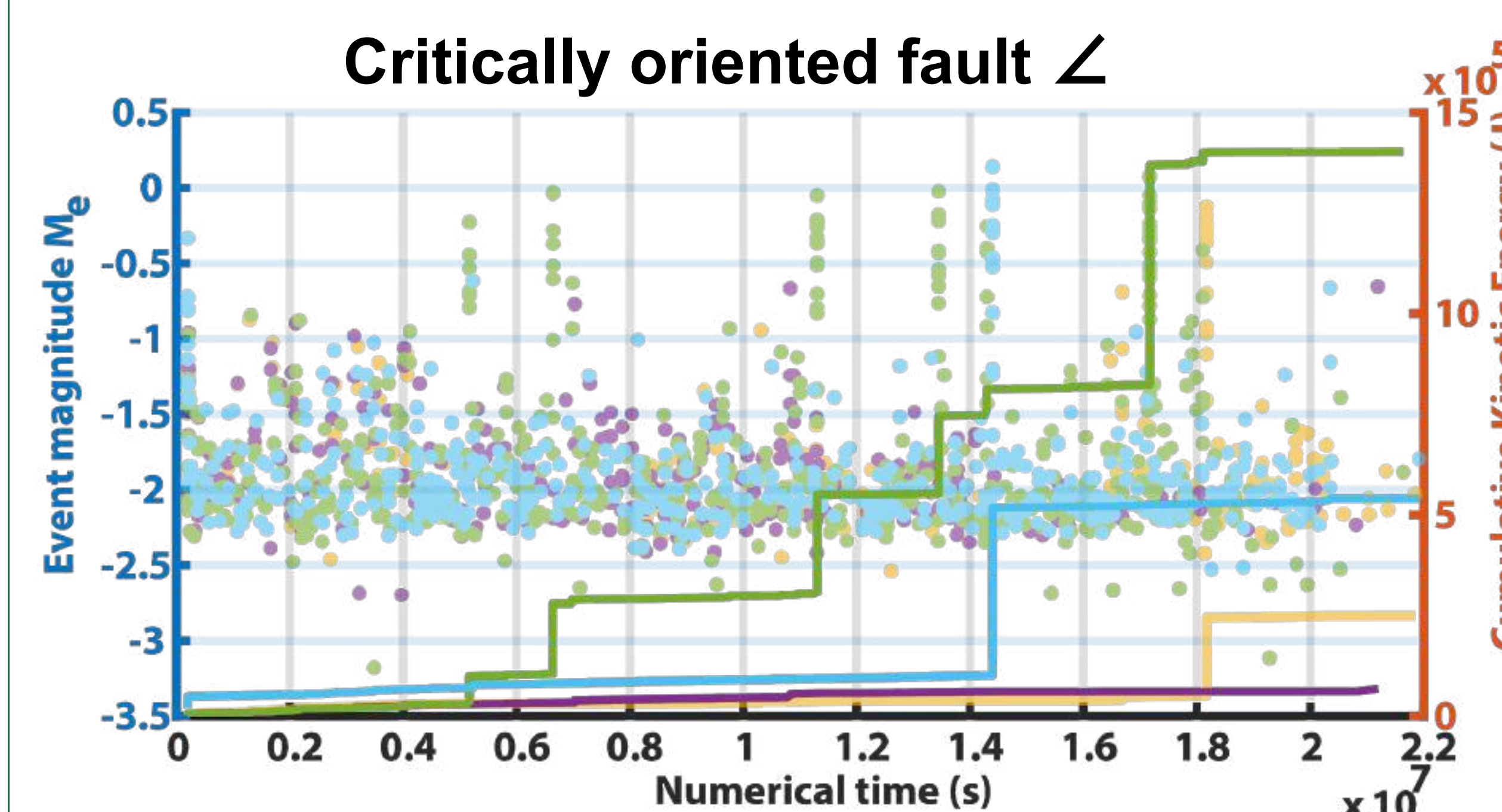
- Skip 2/5 stages to reduce total injected volumes
- Decrease injection spacing to maintain total injected volumes & reduce outward fracture growth

## Fracture Growth and Simulated Microseismics



- Seismic energy is only considered from nucleation of new fractures within the intact rock mass.
- Greater seismic energy is indicative of a more efficient fracturing treatment.

- For both fault orientation (stable  $\perp$  and critical  $\angle$ ) fluids are lost to the fault through fractures.
- For stable fault  $\perp$  fractures are arrested at the fault. Once fluid pressures within the fault are greater than  $\sigma_{min}$  fractures propagate across the fault.



- For unstable fault  $\angle$  fractures are arrested and deviated. Once fluid pressure within the fault are greater than  $\sigma_{min}$  fractures propagate favorably from the edges of the fault.

- For stable fault  $\perp$  skipping stages (3 inj) greatly reduces seismicity, while increasing stages (9 inj) results in greater fluid loss into the fault.
- For unstable fault orientation  $\angle$  skipping stages (3 inj) does not reduce seismicity, while increasing stages (9 inj) results in reduced fluid loss.

## Pressure perturbations

The table below summarizes the maximum fluid pressures at and around the fault at the end of all injections.

Model	Stable oriented fault $\perp$	Critically oriented fault $\angle$
3 injections	57.0 MPa	61.0 MPa
5 injections	59.2 MPa	60.4 MPa
9 injections	58.4 MPa	58.5 MPa
5 injections no fault	60.3 MPa	59.7 MPa

- Higher pressure perturbations would shift the Mohr circle towards the failure envelope with critically oriented faults more likely to fail.

## Conclusion

- For stable faults  $\perp$ , fractures will propagate across the fault once fluid pressures within the fault overcome  $\sigma_{min}$ .
- For unstable faults  $\angle$ , fractures will deviate along the fault. Once fluid pressures overcome  $\sigma_{min}$  fractures will preferably propagate from the edges of the fault.
- For stable faults  $\perp$ , minimizing fractures contact area with the fault results in less fluid loss and less pressurisation of the fault.
- For unstable faults  $\angle$ , decreasing injection spacing results in fewer contact area with the fault due to short and deviated fracture growth near the fault.

## References

Preston, A., Garner, G., Beavis, K., Sadiq, O., & Stricker, S. (2016). Duvernay reserves and resources report: A comprehensive analysis of Alberta's foremost liquids-rich shale resource. *Alberta Energy Regulator, Calgary*, 83.

Pawley, S., Schultz, R., Playter, T., Corlett, H., Shipman, T., Lyster, S., & Hauck, T. (2018). The geological susceptibility of induced earthquakes in the Duvernay play. *Geophysical Research Letters*, 45, 1786–1793.

Eaton, D. (2017). Dynamics of Fault Activation by Hydraulic Fracturing in Overpressured Shales. In *79th EAGE Conference and Exhibition*.

Scientific Review of Hydraulic Fracturing in British Columbia (2019). British Columbia Minister of Energy, Mines, and Petroleum Resources.

Lavoie, V., Willson, S. M., Sturm, C., Lee, J., Purdue, G., & Dempsey, D. (2018, August). A Method to Assess Potential Induced Seismicity Hazard With Application to the Duvernay. In *52nd US Rock Mechanics/Geomechanics Symposium*. American Rock Mechanics Association.

## Acknowledgments

We would like to thank NSERC/CRSNG and the Indian Resource Council for their support. The authors would also like to thank Dr. Jennifer Winter, and Dr. Celia Kennedy for their guidance and support, along with all of the industry contacts. We would also like to thank Geomechanica for providing us with the FDEM Irazu software.

Scholarship recipients and graduates of the NSERC CREATE ReDeveLoP Program under Grant #386133824.